

TS Webinar Series: Fatality Risk Assessment

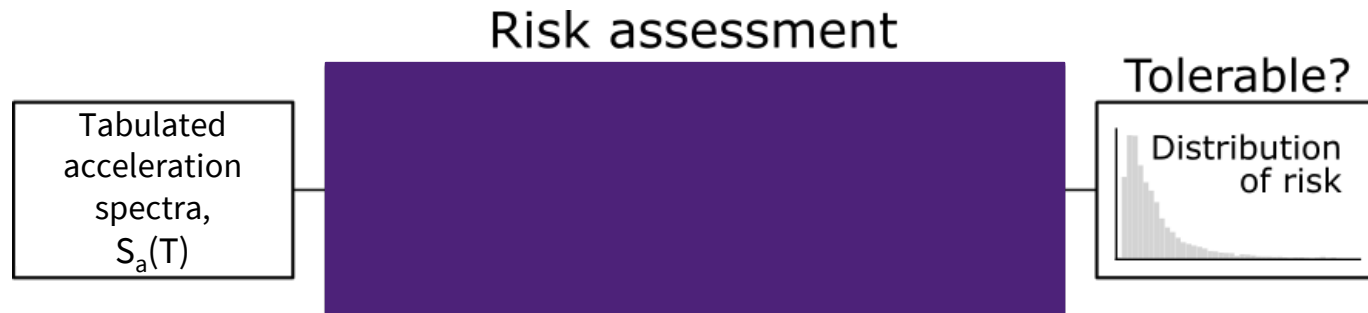
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on behalf of the Seismic Risk Working Group

27 February, 2024

Motivation

“Risk-informed” approach for developing the acceleration spectra

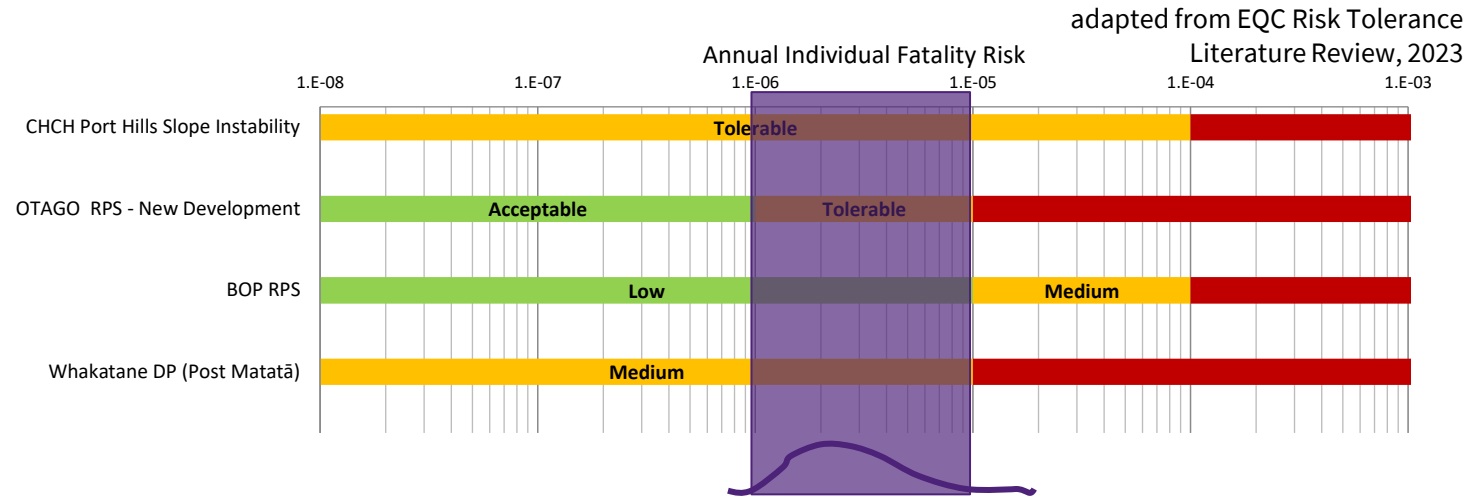


- risk is not the primary driver in developing the spectra, $S_a(T)$
 - assessed as a secondary step to test the risk tolerability
- risk is variable across buildings, informed by many things not just $S_a(T)$
 - not possible to select a strict risk value to target for all buildings

SRWG preliminarily selected a 1/500 annual probability of exceedance (APoE) for ULS, then checked whether the distribution of fatality risk was tolerable.

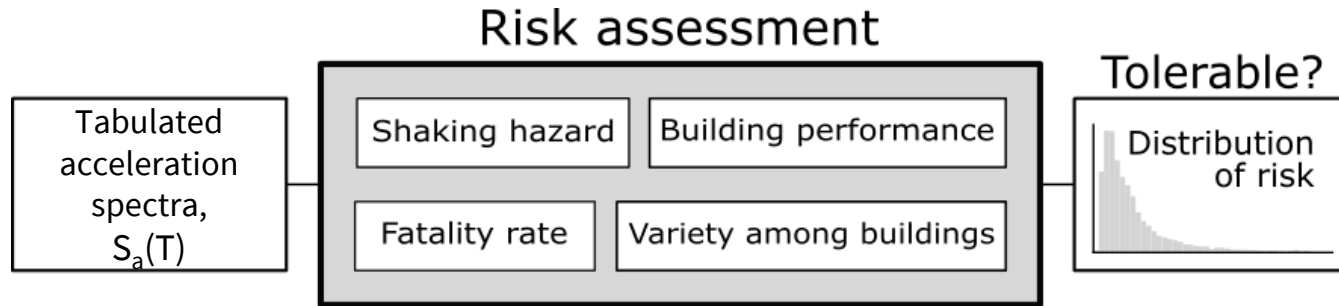
Fatality risk tolerability

Metric: annual individual fatality risk, AIFR

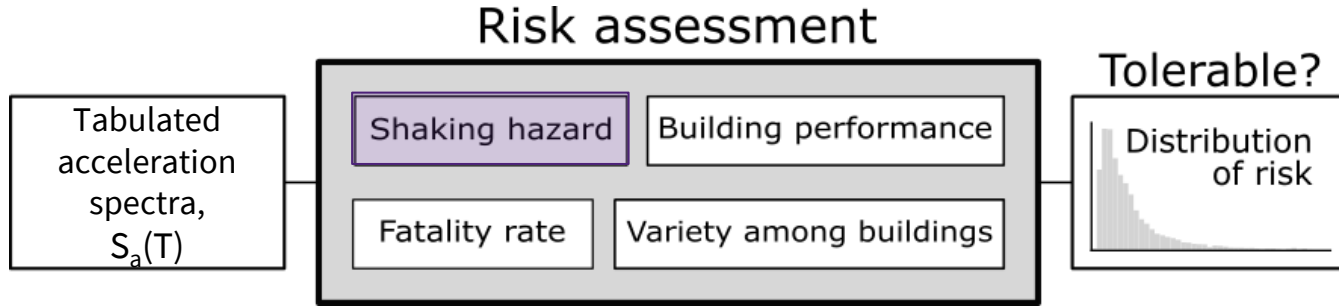


- Risk distribution across all potential code-conforming buildings
 - Should roughly fall between 10^{-6} and 10^{-5}
 - Majority should be well below 10^{-5}

Risk assessment methodology



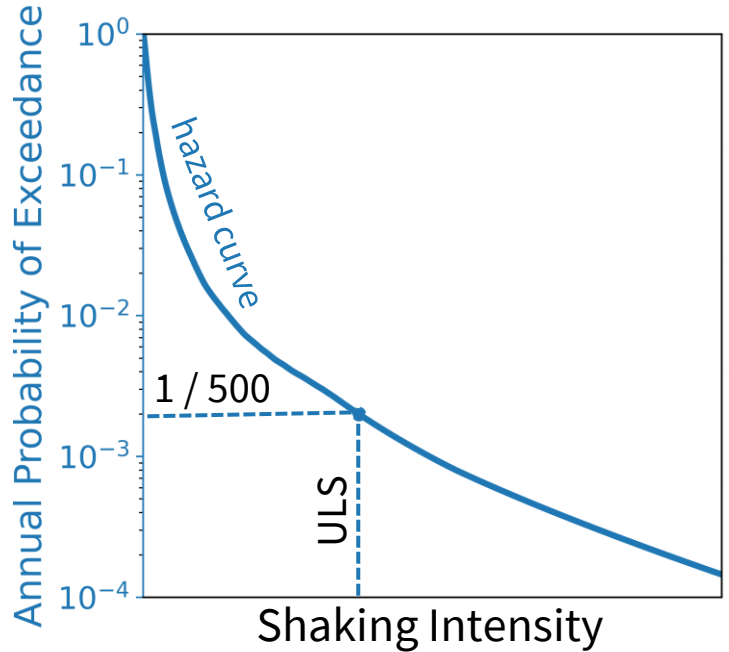
Quantifying the shaking hazard



Site's shaking hazard

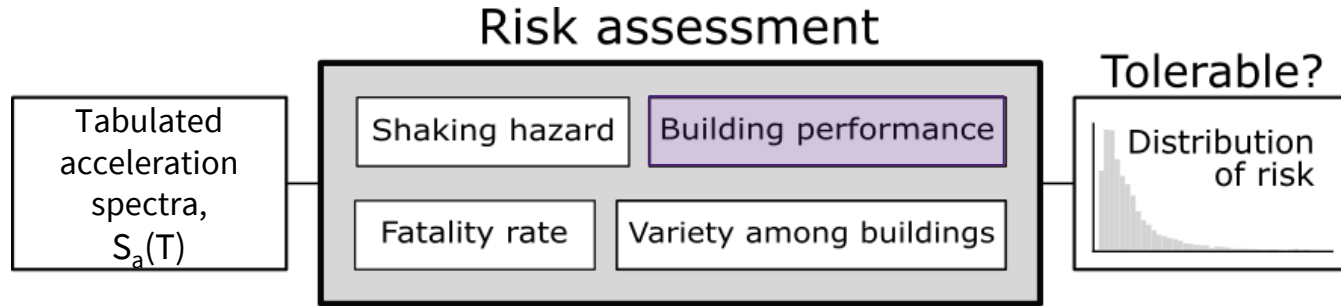
Provided by the NSHM

Probability of shaking for all intensities

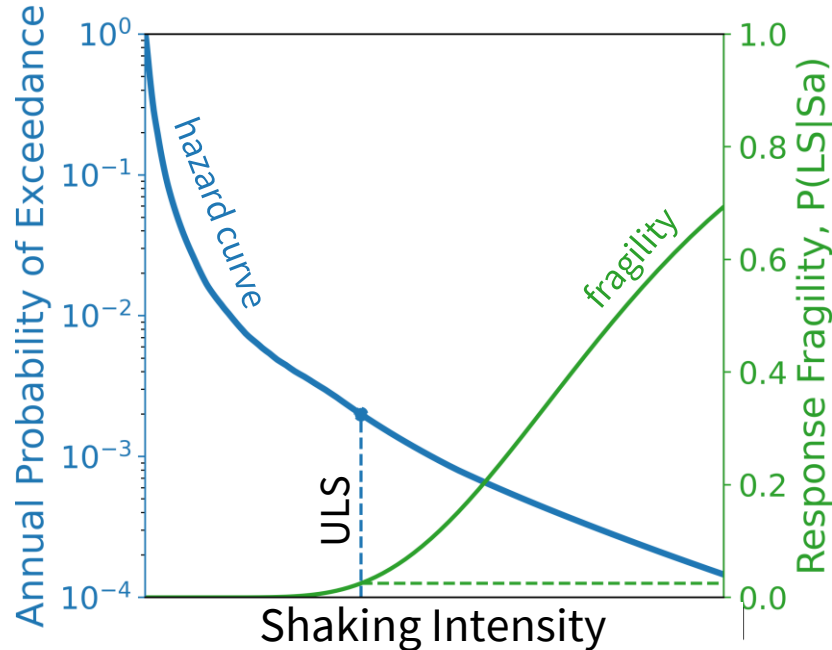


Conceptual figure, not showing x -values

Quantifying the building performance



Site's shaking hazard



Probability of exceeding a limit state, LS

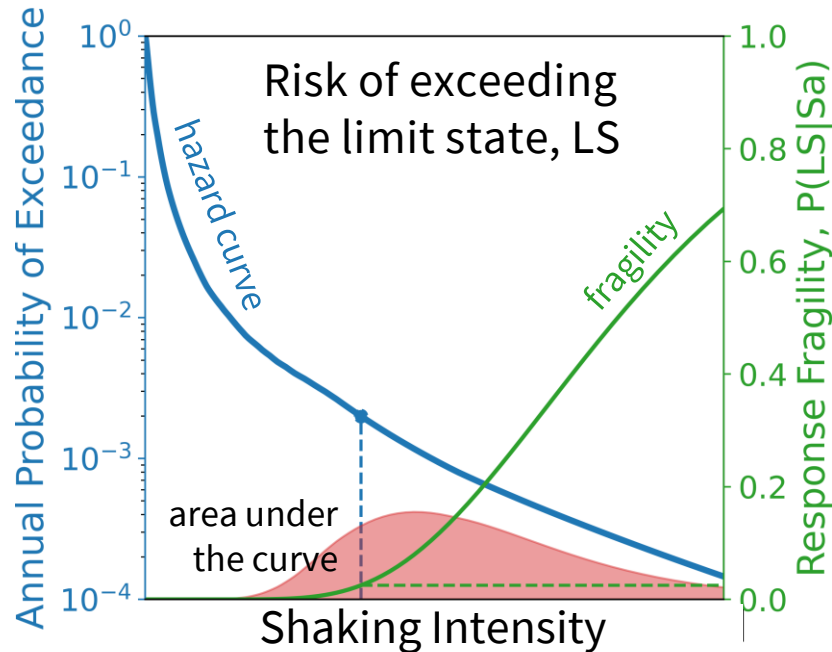
Fragility is linked to the design $S_a(T)$ (ULS)

Probability increases with intensity, steepness defined by uncertainty

Risk calculation



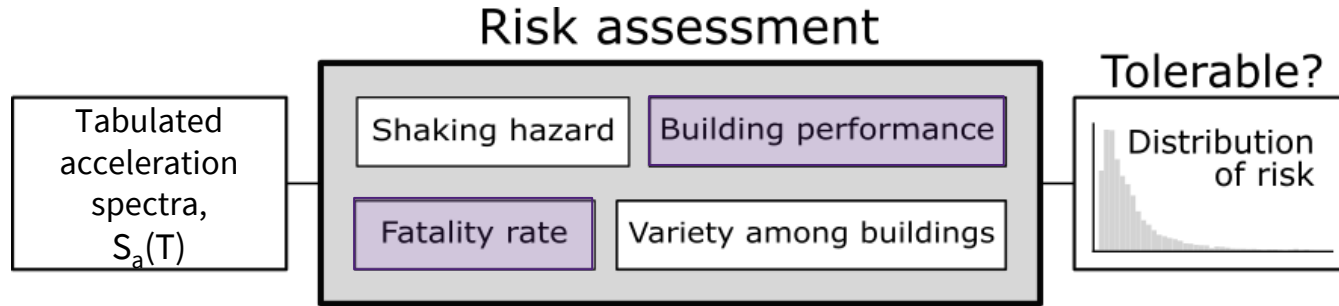
Site's shaking hazard



Probability of exceeding a limit state, LS

Conceptual figure, not showing x -values

Linking fatalities to building performance



Majority of building-related deaths and serious injuries are caused by structural collapse (Horspool et al. 2020)

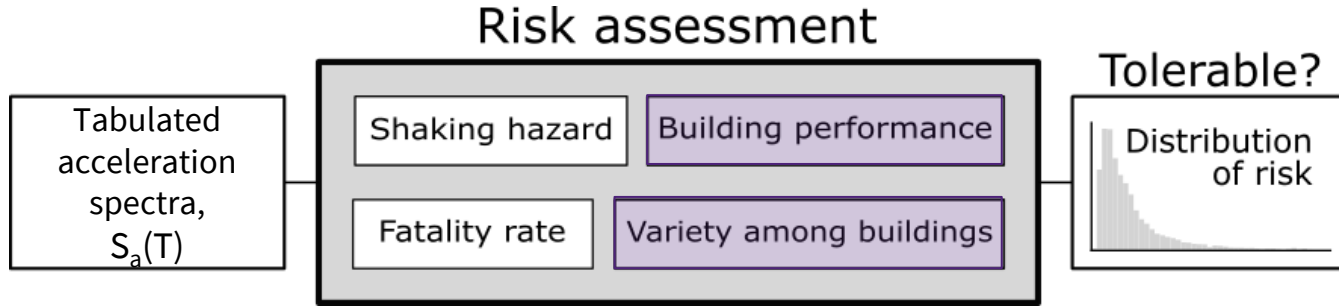
↳ building performance limit state = collapse

Rate of fatality given collapse

- Variable, depending on type of collapse
- Often taken as $P(\text{fatality}|\text{collapse})=10\%$ (e.g. Silva et al. 2016, Horspool et al. 2023)

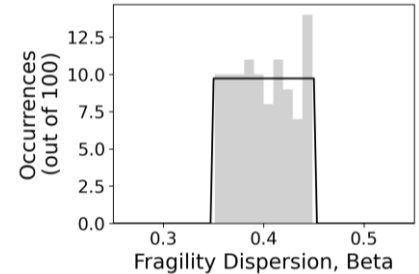
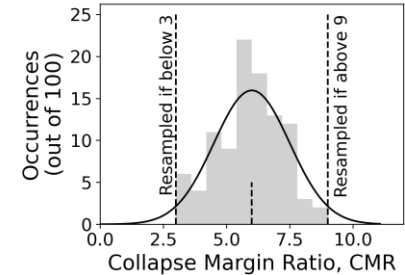
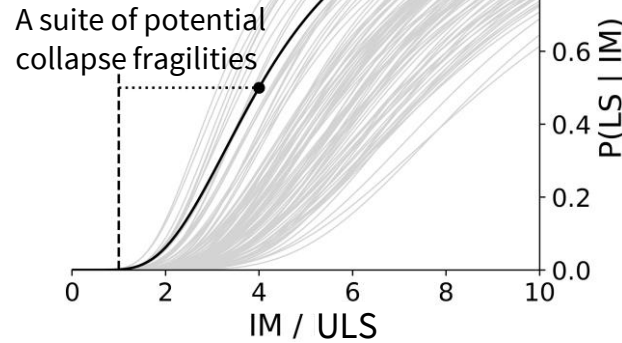
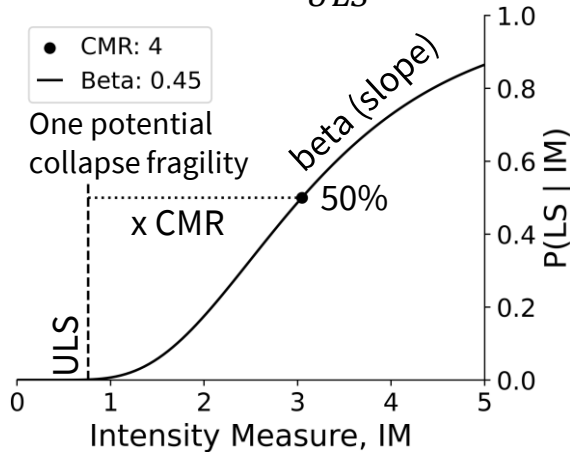
↳ annual collapse risk of 5×10^{-5} becomes AIFR of 5×10^{-6}

Including variability in building performance

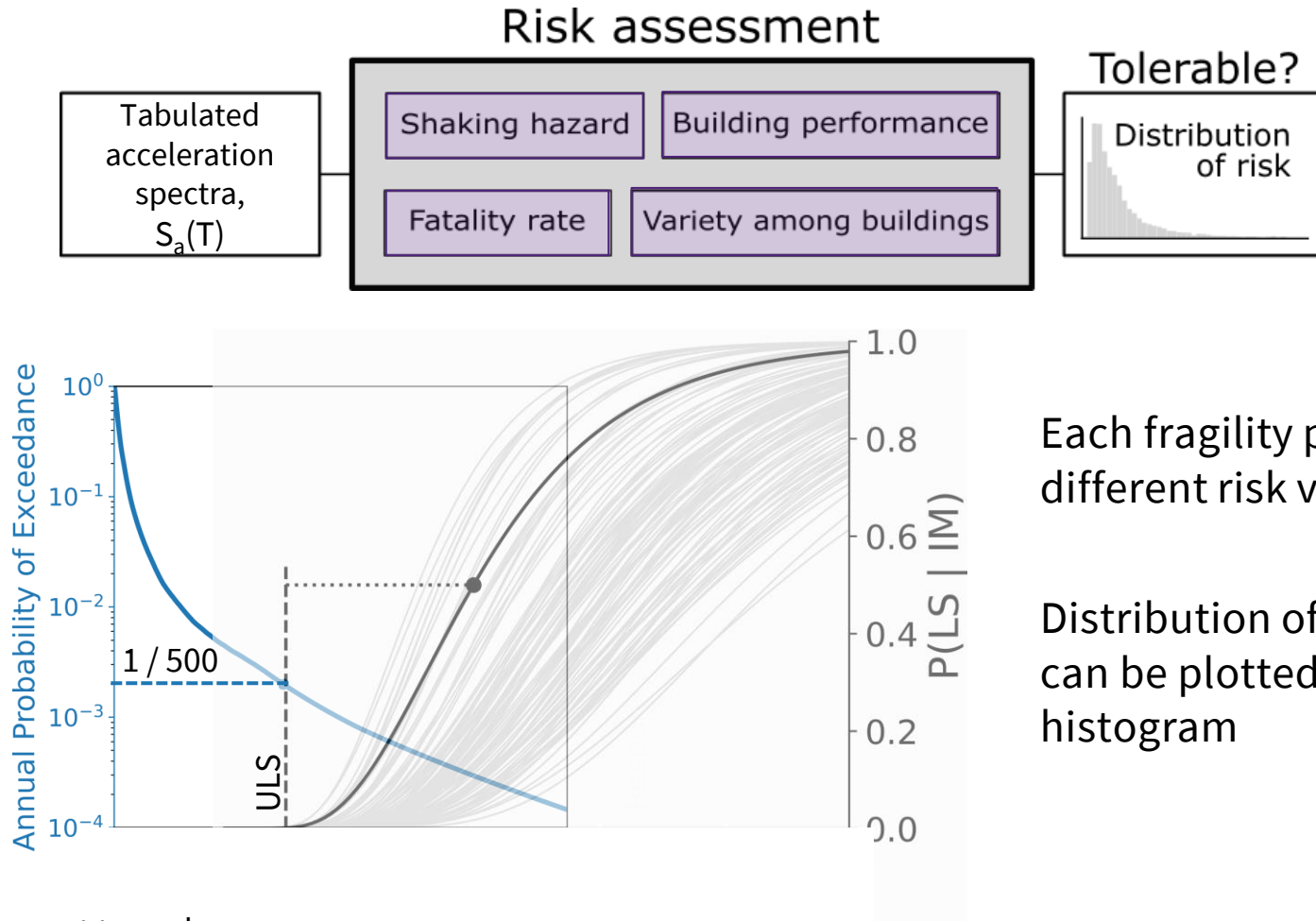


Collapse Margin Ratio,

$$CMR = \frac{IM_{P(C|IM)=50\%}}{ULS}$$



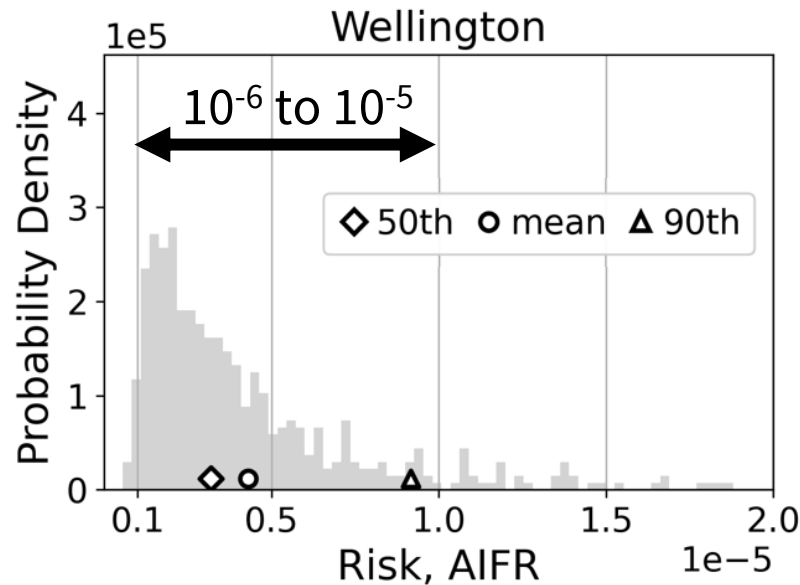
Computing fatality risk for all buildings



* Figures are not to scale

Fatality risk distribution

- Expected distribution of risk among code-conforming buildings
 - Less than 10% extends beyond 1×10^{-5}
 - Majority is below 0.5×10^{-5}



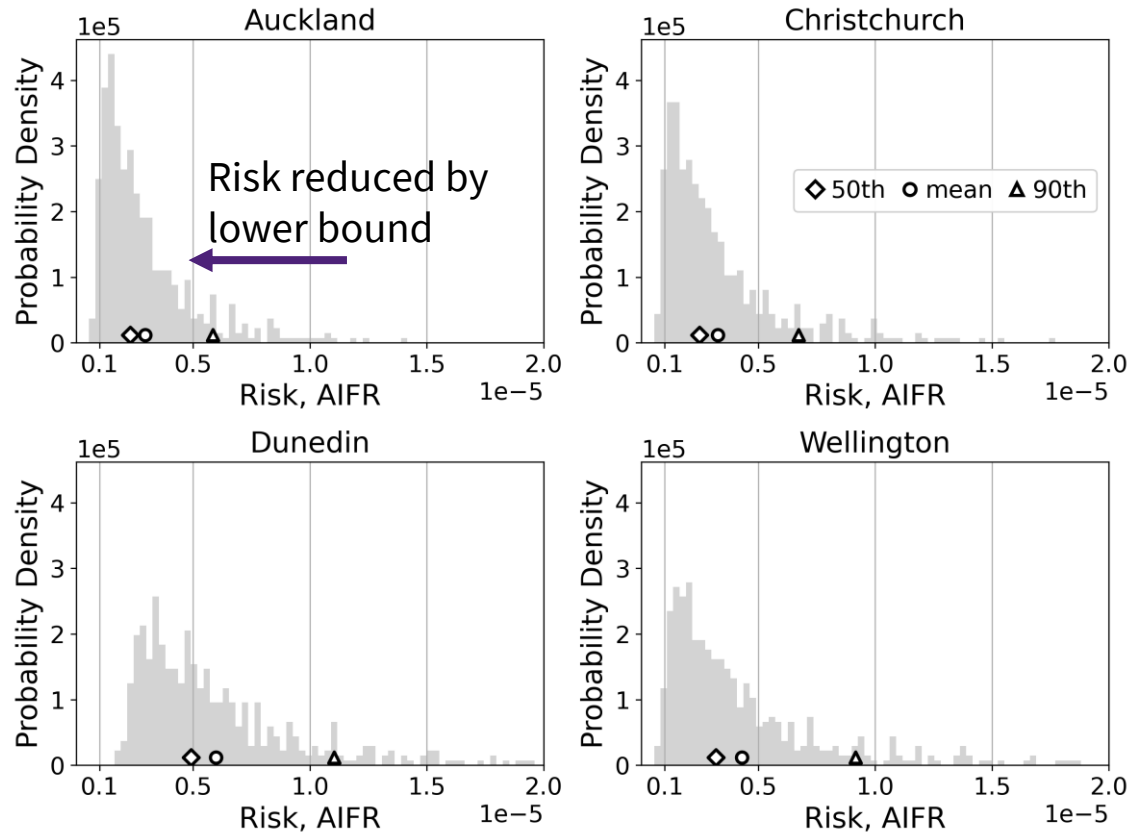
$T = 1.5$ seconds

$V_{s30} = 400$ m/s

$S_a(T)$ for ULS: annual probability of exceedance of 1/500

Fatality risk by location

SA(1.5), Vs30: 400 m/s



- $T = 1.5$ seconds
- $V_{s30} = 400$ m/s
- $S_a(T)$: uniform hazard for an annual probability of exceedance of $1/500$
- Auckland uses the APoE of $1/500$ from the 90th percentile hazard (lower bound that controls in lower hazard)

Conclusion

- Risk is assessed/evaluated after the preliminary $S_a(T)$ development.
- Risk computation includes hazard, building collapse performance, and the likelihood of fatality given collapse
- Risk distribution considers a range of risk across code-conforming buildings
- Majority of risk associated with the ULS $S_a(T)$ is within 10^{-6} to 10^{-5}